

Synthesizing Control Lyapunov-Value Functions for High-Dimensional Systems Using System Decomposition and Admissible Control Sets

Zheng Gong, Hyun Joe Jeong and Sylvia Herbert

Abstract—Control Lyapunov functions (CLFs) play a vital role in modern control applications, but finding them remains a problem. Recently, the control Lyapunov-value function (CLVF) and robust CLVF have been proposed as solutions for nonlinear time-invariant systems with bounded control and disturbance. However, the CLVF suffers from the “curse of dimensionality,” which hinders its application to practical high-dimensional systems. In this paper, we propose a method to decompose systems of a particular coupled nonlinear structure, in order to solve for the CLVF in each low-dimensional subsystem. We then reconstruct the full-dimensional CLVF and provide sufficient conditions for when this reconstruction is exact. Moreover, a point-wise optimal controller can be obtained using a quadratic program. We also show that when the exact reconstruction is impossible, the subsystems’ CLVFs and their “admissible control sets” can be used to generate a Lipschitz continuous CLF. We provide several numerical examples to validate the theory and show computational efficiency.

I. INTRODUCTION

Ensuring stability is one of the most important tasks for autonomous systems operating in the real world. Control Lyapunov functions (CLFs) are energy-like functions that stabilize systems to their equilibrium points [1], [2]. However, it is well known that there lacks a “universal” way of finding CLFs for general nonlinear systems, especially with state or input constraints. Hand-designed and task-specific CLFs have been proposed [3]–[5].

A method to construct control Lyapunov-like functions for nonlinear systems with control and disturbance bounds has been proposed [6], [7]. These control Lyapunov value functions (CLVFs) are based on Hamilton-Jacobi (HJ) reachability analysis [8], [9], and are constructed through dynamic programming. The CLVF guarantees exponential stabilizability, works for general nonlinear dynamics, and deals with state and input constraints well. However, it requires solving a CLVF variational inequality (CLVF-VI) on a discrete grid iteratively, therefore suffering from the “curse of dimensionality.” In the HJ reachability community, many works are proposed to solve this issue, including incorporating reinforcement learning [10], deep learning [11], self-contained subsystems decomposition (SCSD) [12], [13], warming starting [14] and model reduction [15], [16].

The SCSD method provides guaranteed exact solutions for a Hamilton-Jacobi reachability problem under certain assumptions on the coupled nonlinear system and the problem formulation. This approach was further generalized recently through the use of an “admissible control signal

All authors are with the Department of Mechanical and Aerospace Engineering at the University of California, San Diego {zhgong, hj-jeong,sherbert}@ucsd.edu.

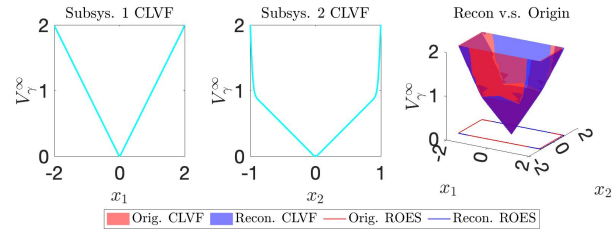


Fig. 1. Original and reconstructed CLVFs for a nonlinear 2D system (13). Left and mid, CLVFs for subsystem 1 and 2, with rates of exponential stabilizability $\gamma = 0.1$. Right, comparison of the reconstructed CLVF and original CLVF, along with their regions of exponential stabilizability (ROES). The reconstructed CLVF is identical to the original CLVF, and the corresponding ROES also matches, validating Lemma 1. The computation time for the original system’s CLVF is 579.12s on a grid of $[-2, 2]$ to $[2, 2]$ with 201 grid points on each dimension. On the same grid, the computation time for the subsystems’ CLVFs are 0.79s and 11.71s. Combined, the decomposition speeds computation time by 48x.

set” (ACSS) [17], which are used to forward propagate and refine the reconstructed value function. This line of work has only been applied to reachability problems, and only provides guarantees on the level sets (reachable sets) of the computed value function, rather than guarantees on the value function itself.

In this work, we generalize the SDSC and ACSS work to numerically compute CLVFs for high dimensional nonlinear control-affine systems with input constraints. The proposed method first applies the standard SCSD and finds the CLVFs for the subsystems. A value function in the original state space is then reconstructed using the subsystems’ CLVFs, and the ACSS is used to determine the domain where this reconstruction is exact (meaning the reconstructed value function is the CLVF for the original system). This is demonstrated in Fig. 1. For systems where exact reconstruction is not possible, the subsystems’ CLVFs and ACSSs can be used to generate a Lipschitz continuous CLF and stabilize the original system. The improved scalability of the proposed method is validated in several numerical examples.

The main contributions of this work are:

- 1) We extend the definition of the ACSS to multi-input systems and to CLVFs, and how it can be constructed.
- 2) We propose a method that combines the SCSD, ACSS, and CLVF, to reconstruct a value function (with CLF properties) for high-dimensional systems whose CLF is not trivial to obtain,
- 3) We provide sufficient conditions on when the reconstruction is exact, i.e., the reconstructed value function

is identical to the CLVF for the original system. The computational complexity of the CLVF for high dimensional systems decreases orders of magnitude.

- 4) For the case when the exact reconstruction is impossible, we show that a Lipschitz continuous CLF can be obtained using the subsystems' CLVFs.
- 5) A quadratic program (QP) is proposed to solve a feedback controller. Further, the ACS is the feasible region of the QP.

II. BACKGROUND

Consider the following nonlinear control-affine system:

$$\frac{dx}{ds} = \dot{x} = f(x) + g(x) \cdot u, \quad s \in [t, 0], \quad x(t) = x_0, \quad (1)$$

where s is the time, $x \in \mathbb{R}^n$ is the state, and $u \in \mathcal{U} \subseteq \mathbb{R}^m$ is the control input, and \mathcal{U} is a compact set. Assume $f : \mathcal{X} \mapsto \mathbb{R}^n$ and $g : \mathcal{X} \mapsto \mathbb{R}^n$ are uniformly continuous, bounded, and Lipschitz continuous in x , and the origin $x^o = \mathbf{0}$ is one uncontrolled equilibrium point, i.e., $f(\mathbf{0}) + g(\mathbf{0}) \cdot \mathbf{0} = 0$. Further assume the control signal $u(\cdot)$ is drawn from measurable control functions:

$$u(\cdot) \in \mathbb{U} := \{u : [t, 0] \mapsto \mathcal{U}, u(\cdot) \text{ is measurable}\}.$$

Under these assumptions, we can solve for a unique solution of (1), denoted as $\xi(s; t, x, u(\cdot))$ (in short $\xi(s)$).

A. CLF and CLVF

A function $V : \mathbb{R}^n \mapsto \mathbb{R}$ is a local CLF of the equilibrium point x^o if, in a neighborhood \mathcal{O} of x^o , the following holds: (a) V is proper, (b) V is positive definite and continuously differentiable in \mathcal{O} , and (c) $\forall x \in \mathcal{O}, \exists u \in \mathcal{U}$, s.t. $\dot{V} = \frac{dV}{dx} \cdot [f(x) + g(x)u] < 0$.

Finding CLF is hard. Recently, [6] proposed the CLVF, which has CLF properties and can be obtained numerically, formally defined below.

Definition 1: Given the following function

$$V_\gamma(x, t) = \min_{u \in \mathbb{U}} \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s)), \quad (2)$$

the CLVF $V_\gamma^\infty : D_\gamma \mapsto \mathbb{R}$ of (1) is the limit function:

$$V_\gamma^\infty(x) = \lim_{t \rightarrow -\infty} V_\gamma(x, t). \quad (3)$$

Here, $\ell(x)$ is the loss function, normally chosen to be vector norms, γ is a user-specified parameter that represents the desired exponential decay rate. The domain of the CLVF is given as $D_\gamma \subseteq \mathbb{R}^n$. Since (2) is time-dependent, it is called the time-varying CLVF (TV-CLVF).

Proposition 2 of [6] shows there exists $u \in \mathcal{U}$ s.t.

$$\dot{V}_\gamma^\infty(x) \leq \gamma V_\gamma^\infty(x), \quad \forall x \in D_\gamma. \quad (4)$$

Note that since we assume the system has an equilibrium point, the definition of CLVF is simplified compared to [6]. The CLVF value of a state captures the largest exponentially amplified deviation between the origin and the trajectory starting from that state. If this is finite, then there must exist some control signal for which the system trajectory

converges to the origin at the same rate γ . The domain of the CLVF D_γ is also known as the region of exponential stabilizability (ROES). A larger γ results in a faster convergence to the origin, but a smaller ROES.

Under the scope of this paper, the CLVF is a Lipschitz continuous CLF, while the main difference is that using CLVF, the user can trade off between a faster convergence or a larger ROES.

It has been shown that the TV-CLVF is the unique viscosity solution to the following CLVF-VI,

$$0 = \max \left\{ \ell(x) - V_\gamma(x, t), \right. \\ \left. D_t V_\gamma + \min_{u \in \mathcal{U}} D_x V_\gamma \cdot (f(x) + g(x) \cdot u) + \gamma V_\gamma(x, t) \right\}, \quad (5)$$

with terminal condition $V_\gamma(x, 0) = \ell(x)$. The CLVF can be obtained by solving this VI backward in time until convergence. Here, D_t denotes the time derivative, and D_x denotes the gradient with respect to x .

B. System decomposition and ACS

Definition 2: (SCSD) Given (1) and assume there exists state partitions $z_1 = (x_1; x_c) \in \mathcal{Z}_1, z_2 = (x_2; x_c) \in \mathcal{Z}_2$, where $x_1 \in \mathbb{R}^{n_1}, x_2 \in \mathbb{R}^{n_2}, x_c \in \mathbb{R}^{n_c}, n_1, n_2 > 0, n_c \geq 0, n_1 + n_2 + n_c = n$. Assume also the control inputs can be partitioned similarly with $v_1 = (u_1; u_c) \in \mathcal{V}_1, v_2 = (u_2; u_c) \in \mathcal{V}_2$, where $u_1 \in \mathbb{R}^{m_1}, u_2 \in \mathbb{R}^{m_2}, u_c \in \mathbb{R}^{m_c}$ and $m_1 + m_2 + m_c = m$. The two self-contained subsystems of (1) are

$$\dot{z}_1 = f_1(z_1) + g_1(z_1)v_1, \quad \dot{z}_2 = f_2(z_2) + g_2(z_2)v_2, \quad (6)$$

with corresponding solution $\phi_1(s), \phi_2(s)$.

When x_c or/and u_c exist, we say the subsystems are coupled through the common states x_c or/and controls u_c , and they have shared states or/and controls. The shared controls are one of the main causes of the inconsistency between the reconstructed value function and the original value function.

Remark 1: After decomposition, if the subsystems only have shared states, but no shared controls, then the shared states must be autonomous, i.e., $\dot{x}_c = f_c(x_c)$. This means the control has no impact on the shared states. In other words, starting from the same initial condition, the trajectory of the shared states is the same in all subsystems. On the other hand, if the subsystems have shared control, they must also have shared states.

To build the connection between the state and control of the subsystems and the state and control of the original system, we define the projection and back projection operator.

Definition 3: (Projection and back projection operators.) A **state projection operator** $\mathcal{P}_{x,i} : \mathbb{R}^n \mapsto \mathbb{R}^{n_i+n_c}$ maps a state $x \in \mathbb{R}^n$ to a state $z_i \in \mathbb{R}^{n_i+n_c}$:

$$\mathcal{P}_{x,i}(x) := (x_i, x_c) = z_i.$$

A **control projection operator** $\mathcal{P}_{u,i} : \mathbb{R}^m \mapsto \mathbb{R}^{m_i+m_c}$ maps a control $u \in \mathbb{R}^m$ to a control $v_i \in \mathbb{R}^{m_i+m_c}$:

$$\mathcal{P}_{u,i}(u) := (u_i, u_c) = v_i.$$

A **state back projection operator** $\mathcal{P}_{x,i}^{-1} : \mathbb{R}^{n_i+n_c} \mapsto \mathbb{R}^n$ maps a state $z_i \in \mathbb{R}^{n_i+n_c}$ to a set of states $x \in \mathbb{R}^n$:

$$\mathcal{P}_{x,i}^{-1}(z_i) := \{x \in \mathcal{X} : (x_i, x_c) = z_i\}.$$

A **control back projection operator** $\mathcal{P}_{u,i}^{-1} : \mathbb{R}^{m_i+m_c} \mapsto \mathbb{R}^m$ maps a control $v_i \in \mathbb{R}^{m_i+m_c}$ to a set of controls $u \in \mathbb{R}^m$:

$$\mathcal{P}_{u,i}^{-1}(v_i) := \{u \in \mathcal{U} : (u_i, u_c) = v_i\}.$$

Following [17], we define the ACS for the TV-CLVF.

Definition 4: The ACS of (2) is the set of all the control signals such that the corresponding trajectory achieves the same value $V_\gamma(x, t)$:

$$\mathbb{U}_a(x, t) = \{u(\cdot) \in \mathbb{U} : \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s; t, x, u(\cdot))) = V_\gamma(x, t)\}$$

The ACS cannot be obtained directly, but we could numerically construct one admissible control signal. Using (5), define the ACS given a time step δt

$$\mathcal{U}_a(x, t) = \{u \in \mathcal{U} : V_\gamma(x, t - \delta t) - V_\gamma(x, t) - (D_x V_\gamma \cdot (f(x) + g(x) \cdot u) + \gamma V_\gamma(x, t)) \delta t \geq 0\}. \quad (7)$$

The ACS is the set of control inputs, using which the one-step decrease of the value is achieved. One admissible control signal $u_a(\cdot)$ for x can be computed by concatenating the ACSs over time: $u_a(\cdot) = [u_{a,s_1}, u_{a,s_2}, \dots, u_{a,0}]$, where $u_{a,s_i}(\cdot) \in \mathcal{U}_a(\xi(s_i), s_i)$.

Both the ACS and ACS are guaranteed to be non-empty [17], and they can be similarly defined for subsystems.

III. PROBLEM FORMULATION AND APPROACH

In this section, we begin with an idealized case, where the system can be decomposed into two subsystems with no shared control, and show the reconstructed value function is the CLVF for the original system. This is called *exact reconstruction*. We then provide a sufficient condition of exact reconstruction for cases where subsystems are coupled through shared controls. Further, for systems where an exact reconstruction is impossible, we apply the concept of ACS, and show how the reconstructed value function is a Lipschitz continuous CLF. All theorems follow naturally to the cases where the original system is decomposed into more than two subsystems.

Denote the TV-CLVF of the two subsystems as

$$V_{\gamma,i}(z_i, t) = \min_{v_i \in \mathbb{V}_i} \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell_i(\phi_i(s)), \quad i = 1, 2,$$

and the CLVF for subsystems as $V_{\gamma,i}^\infty : \mathcal{D}_{\gamma,i} \subseteq \mathcal{Z}_i \mapsto \mathbb{R}$,

$$V_{\gamma,i}^\infty(z_i) = \lim_{t \rightarrow -\infty} V_{\gamma,i}(z_i, t), \quad i = 1, 2.$$

For clarity, the CLVF computed directly for the high-dimensional system (1) is called the *original CLVF*, while the CLVF (TV-CLVF) reconstructed from subsystems is called the *reconstructed CLVF (TV-CLVF)*, denoted as $\bar{V}_\gamma^\infty(x)$ ($\bar{V}_\gamma(x, t)$). The domain of $\bar{V}_\gamma^\infty(x)$ is denoted by $\bar{\mathcal{D}}_\gamma$.

Using (7), the ACS can be solved:

$$D_x V_\gamma(x, t) g(x) \cdot u \leq \frac{V_\gamma(x, t - \delta t) - V_\gamma(x, t)}{\delta t} - \gamma V_\gamma(x, t) - D_x V_\gamma(x, t) f(x), \quad (8)$$

which is a linear inequality for single-input systems, and a half-space for multi-input systems. Though we cannot get an analytic solution of this half-space, it is numerically easy to obtain one element of it.

A. Exact Reconstruction of the CLVF

In this section, we assume $\ell(x) = \max(\ell_1(z_1), \ell_2(z_2))$, meaning the loss function for the original system equals the reconstructed loss function from subsystems. One possible choice is $\ell_i(z_i) = \|z_i\|_\infty$. Two results are provided here, showing the sufficient conditions for exact reconstruction of the CLVF, without shared controls (Lemma 1) and with shared controls (Theorem 2).

Define $\bar{V}_\gamma^\infty(x) = \max(V_{\gamma,1}^\infty(z_1), V_{\gamma,2}^\infty(z_2))$, where $z_1 = \mathcal{P}_{x,1}(x)$, $z_2 = \mathcal{P}_{x,2}(x)$, and $\bar{\mathcal{D}}_\gamma = \mathcal{P}_{x,1}^{-1}(\mathcal{D}_{\gamma,1}) \cap \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,2})$. Then we have:

Lemma 1: Assume there are no common controls after decomposition. Then, $\bar{V}_\gamma^\infty(x) = V_\gamma^\infty(x)$ and $\bar{\mathcal{D}}_\gamma = \mathcal{D}_\gamma$.

Proof: Define $\bar{V}_\gamma(x, t) = \max(V_{\gamma,1}(z_1, t), V_{\gamma,2}(z_2, t))$, we first show $\bar{V}_\gamma(x, t) = V_\gamma(x, t)$ by contradiction.

Assume $\bar{V}_\gamma(x, t) < V_\gamma(x, t)$, then there exists optimal control signals $u^*(\cdot) \in \mathbb{U}$, $v_1^*(\cdot) \in \mathbb{V}_1$ and $v_2^*(\cdot) \in \mathbb{V}_2$, s.t.

$$\begin{aligned} & \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s; t, x, u^*(\cdot))) \\ & > \max\left(\max_{s \in [t, 0]} e^{\gamma(s-t)} \ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \right. \\ & \quad \left. \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot)))\right) \\ & = \max_{s \in [t, 0]} \max\left(e^{\gamma(s-t)} \ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \right. \\ & \quad \left. e^{\gamma(s-t)} \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot)))\right) \\ & = \max_{s \in [t, 0]} e^{\gamma(s-t)} \max\left(\ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \right. \\ & \quad \left. \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot)))\right). \quad (9) \end{aligned}$$

Since the two subsystems have no shared controls, we could reconstruct one trajectory for (1) using the back projection: $\bar{\xi}(s) = \mathcal{P}_{x,1}^{-1}(\phi_1(s)) \cap \mathcal{P}_{x,2}^{-1}(\phi_2(s))$. Since the shared states evolve independent of the controls applied, (9) becomes

$$\begin{aligned} & \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s; t, x, u^*(\cdot))) \\ & > \max_{s \in [t, 0]} e^{\gamma(s-t)} \max\left(\ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \right. \\ & \quad \left. \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot)))\right) \\ & = \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\bar{\xi}(s; t, x, u^*(\cdot))). \end{aligned}$$

This means $u^*(\cdot)$ is not optimal, which is a contradiction.

Similarly, assume $\bar{V}_\gamma(x, t) > V_\gamma(x, t)$, then there also exists optimal control signals $u^*(\cdot) \in \mathbb{U}$, $v_1^*(\cdot) \in \mathbb{V}_1$ and

$v_2^*(\cdot) \in \mathbb{V}_2$, s.t.

$$\begin{aligned} & \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s; t, x, u^*(\cdot))) \\ & < \max_{s \in [t, 0]} e^{\gamma(s-t)} \max(\ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \\ & \quad \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot))))). \end{aligned} \quad (10)$$

This is obtained following the same procedure as (9). However, projecting $\xi(s)$ into the two subsystems spaces, we get $\bar{\phi}_1(s) = \mathcal{P}_{x,1}(\xi(s))$, $\bar{\phi}_2(s) = \mathcal{P}_{x,2}(\xi(s))$, and we have

$$\begin{aligned} & \max_{s \in [t, 0]} e^{\gamma(s-t)} \ell(\xi(s; t, x, u^*(\cdot))) \\ & = \max_{s \in [t, 0]} e^{\gamma(s-t)} \max(\ell_1(\bar{\phi}_1(s)), \ell_2(\bar{\phi}_2(s))). \end{aligned}$$

Using (10), we have

$$\begin{aligned} & \max_{s \in [t, 0]} e^{\gamma(s-t)} \max(\ell_1(\bar{\phi}_1(s)), \ell_2(\bar{\phi}_2(s))) \\ & < \max_{s \in [t, 0]} e^{\gamma(s-t)} \max(\ell_1(\phi_1(s; t, z_1, v_1^*(\cdot))), \\ & \quad \ell_2(\phi_2(s; t, z_2, v_2^*(\cdot))))), \end{aligned}$$

which shows that either v_1^* or v_2^* is not optimal. Combined, we have shown that $\forall t \leq 0$, $x \in \mathbb{R}^n$, $V_\gamma(x, t) = \bar{V}_\gamma(x, t)$. Next we show that $\bar{V}_\gamma^\infty(x) = V_\gamma^\infty(x)$.

Since the CLVF exists for two subsystems, we have

$$\begin{aligned} V_\gamma^\infty(x) &= \lim_{t \rightarrow -\infty} V_\gamma(x, t) \\ &= \lim_{t \rightarrow -\infty} \bar{V}_\gamma(x, t) \\ &= \lim_{t \rightarrow -\infty} \max(V_{\gamma,1}(z_1, t), V_{\gamma,2}(z_2, t)) \\ &= \max\left(\lim_{t \rightarrow -\infty} V_{\gamma,1}(z_1, t), \lim_{t \rightarrow -\infty} V_{\gamma,2}(z_2, t)\right) \\ &= \max(V_{\gamma,1}^\infty(z_1), V_{\gamma,2}^\infty(z_2)) = V_\gamma(x). \end{aligned}$$

This also shows that $\mathcal{D}_\gamma \supseteq \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,1}) \cap \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,2})$.

Assume $\exists x \notin \mathcal{D}_\gamma$, $x \in \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,1}) \cap \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,2})$. This means the optimal trajectory ξ starting from x satisfies the following two condition simultaneously: 1) $V_\gamma^\infty(x)$ is infinite and 2) both $V_{\gamma,1}^\infty(z_1)$ and $V_{\gamma,2}^\infty(z_2)$ are finite. This is a contradiction. Therefore, we have $\mathcal{D}_\gamma = \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,1}) \cap \mathcal{P}_{x,2}^{-1}(\mathcal{D}_{\gamma,2})$. ■

Lemma 1 shows that if there exists no shared control, the reconstructed value function is the CLVF, and their domains are also the same. This means system (1) can be exponentially stabilized to the origin from \mathcal{D}_γ .

Remark 2: Numerically, Lemma 1 is easy to implement: after decomposition, it is easy to check if all subsystems have shared controls. If Lemma 1 is applicable, we simply compute the CLVF for the subsystems and take the max to reconstruct the CLVF for the original system.

The essence of this proof is that the optimal control signal (with respect to (3)) for the original system can always be reconstructed from the subsystems' optimal control signals, i.e. $u^*(\cdot) = [v_1^*(\cdot); v_2^*(\cdot)]$, and that the projection and back projection between the original system's trajectory and subsystems' trajectories are both unique. This is guaranteed because there is no shared control. However,

many practical systems cannot be decomposed into fully independent subsystems. From Remark 1, if there are shared controls, there must also be shared states. If two subsystems require conflicting values of the shared control(s), the back projection of subsystems' trajectories cannot reconstruct the original system's trajectory.

For the subsystems, denote the ACSS as $\mathbb{U}_{a,1}(z_1, t)$ and $\mathbb{U}_{a,2}(z_2, t)$, and their shared control component as $\mathbb{U}_{a,1}^c(z_1, t)$ and $\mathbb{U}_{a,2}^c(z_2, t)$. The ACSS for (1) can be reconstructed as

$$\begin{aligned} \bar{\mathbb{U}}_a(x, t) &= \mathcal{P}_{u,1}^{-1}(\mathbb{U}_{a,1}(\mathcal{P}_{x,1}(x), t)) \cap \mathcal{P}_{u,2}^{-1}(\mathbb{U}_{a,2}(\mathcal{P}_{x,2}(x), t)) \\ \bar{\mathbb{U}}_a^c(x, t) &= \mathbb{U}_{a,1}^c(\mathcal{P}_{x,1}(x), t) \cap \mathbb{U}_{a,2}^c(\mathcal{P}_{x,2}(x), t). \end{aligned}$$

Note that though $\mathbb{U}_{a,1}^c(z_1, t)$ and $\mathbb{U}_{a,2}^c(z_2, t)$ are non-empty, $\bar{\mathbb{U}}_a^c(x, t)$ might be empty for some x .

Remark 3: $\bar{\mathbb{U}}_a(x, t)$ is non-empty if and only if $\bar{\mathbb{U}}_a^c(x, t)$ is non-empty.

Now, we provide one sufficient condition on exact reconstruction for the case with shared controls.

Theorem 2: Assume $\bar{\mathbb{U}}_a^c(x, t)$ is non-empty for all $t \leq 0$ and $x \in \mathcal{S}_\gamma$, where \mathcal{S}_γ is some level set of $\bar{V}_\gamma^\infty(x)$. Then, $\bar{V}_\gamma^\infty(x) = V_\gamma^\infty(x)$ on \mathcal{S}_γ .

Proof: The proof can be obtained similarly to Lemma 1. If $\bar{\mathbb{U}}_a^c(x, t)$ is non-empty for all $t \leq 0$, $x \in \mathcal{S}_\gamma$, then given the subsystems' trajectories $\phi_1(s)$ and $\phi_2(s)$, a trajectory of (1) can again be reconstructed as

$$\bar{\xi}(s) = \mathcal{P}_{x,1}^{-1}(\phi_1(s)) \cap \mathcal{P}_{x,2}^{-1}(\phi_2(s)).$$

Similarly, given a trajectory $\xi(s)$ of (1), the two subsystems' trajectories can be obtained as

$$\bar{\phi}_1(s) = \mathcal{P}_{x,1}(\xi(s)), \quad \bar{\phi}_2(s) = \mathcal{P}_{x,2}(\xi(s)).$$

Therefore, assume $\bar{V}_\gamma(x, t) < V_\gamma(x, t)$, we can obtain (9), and assume $\bar{V}_\gamma(x, t) > V_\gamma(x, t)$, we can obtain (10). In other words, $\forall x \in \mathcal{S}_\gamma$, we again construct two contradictions to show that $\bar{V}_\gamma(x, t) < V_\gamma(x, t)$ and $\bar{V}_\gamma(x, t) > V_\gamma(x, t)$ cannot happen. The remaining steps are identical to the proof of Lemma 1. ■

A direct implication of Theorem 2 is that the reconstructed ACSS (if not empty) is always equal to the ACSS directly computed for (1). In other words, if $\bar{\mathbb{U}}_a^c(x, t)$ is non-empty for all $t \leq 0$ and $x \in \mathcal{S}_\gamma$, then $\bar{\mathbb{U}}_a^c(x, t) = \mathbb{U}_a^c(x, t)$. We provide the following standard results without proof.

Proposition 1: System (1) can be exponentially stabilized to the origin from \mathcal{S}_γ .

The numerical implementation of Theorem 2 is shown in Alg. 1. The convergence time for the subsystems may differ, therefore, after one TV-CLVF converges, we repeat its final value until the other subsystem's CLVF converges. Further, since the TV-CLVF is computed backward in time, we reverse the time vector of the TV-CLVF ($V_\gamma(x, t) = V_\gamma(x, T - t)$) to forward propagate the trajectory.

Alg. 1 has a maximum iteration $\frac{T}{\delta t}$, where T is the convergence time. It first computes the ACS from the subsystem's value function and reconstructs the ACS for (1). Then, it checks if the shared control component of the ACS

Algorithm 1 Exact reconstruction with shared controls

Require: Subsystems TV-CLVF $V_{\gamma,i}$, convergence time T , time step δt

- 1: **Initialization:** $t \leftarrow T$, \mathcal{T}_γ empty
 - 2: **Output:** $V_\gamma^\infty(x)$ and domain \mathcal{S}_γ
 - 3: Reverse time of TV-CLVFs
 - 4: **for** all grids point x **do**
 - 5: **while** $t \neq 0$ **do**
 - 6: Compute the subsystems ACS $\mathcal{U}_{a,1}, \mathcal{U}_{a,2}$ using (8)
 - 7: Get the **shared control component** $\mathcal{U}_{a,1}^c, \mathcal{U}_{a,2}^c$ and other component $\mathcal{U}_{a,1}^o, \mathcal{U}_{a,2}^o$
 - 8: $\mathcal{U}_a^c(x, t) \leftarrow \mathcal{U}_{a,1}^c(\text{proj}_1(x), t) \cap \mathcal{U}_{a,2}^c(\text{proj}_2(x), t)$
 - 9: **if** $\mathcal{U}_a^c(x, t)$ empty **then** Break
 - 10: **else if** $\mathcal{U}_a^o(x, t)$ not empty **then**
 - 11: $u_c \in \mathcal{U}_{a,1}^o(x, t), u_1 \in \mathcal{U}_{a,1}^o, u_2 \in \mathcal{U}_{a,2}^o$
 - 12: $u \leftarrow [u_1, u_2, u_c]$
 - 13: $x \leftarrow x + [f(x) + g(x) \cdot u] \delta t$
 - 14: $t \leftarrow t + \delta t$
 - 15: **end if**
 - 16: **end while**
 - 17: $V_\gamma^\infty(x) \leftarrow \max(V_{\gamma,1}^\infty(z_1, 0), V_{\gamma,2}^\infty(z_2, 0))$, add x to \mathcal{T}_γ
 - 18: **end for**
 - 19: $\mathcal{S}_\gamma \leftarrow$ largest level set of $V_\gamma^\infty(x)$ contained in \mathcal{T}_γ
-

is empty. If not empty, it applies one random control input from ACS, updates the state, and repeats. For any initial state whose ACS is non-empty along the whole trajectory, concatenating the control used, we get one admissible control signal. This state is added to a set \mathcal{T}_γ , and \mathcal{S}_γ is the largest level set of $\bar{V}_\gamma^\infty(x)$ contained in \mathcal{T}_γ . Note that we take the maximum between $V_{\gamma,1}^\infty(z_1, 0)$ and $V_{\gamma,2}^\infty(z_2, 0)$. This is because we reverse the time vector at line 3.

Remark 4: Assume the original system is n -dimension, and each dimension has N grid points, the computation complexity is of $\mathcal{O}(N^n)$. Assume it is decomposed into p m -dimension subsystems (where $m < n$), and assume each dimension still have the same N grid points, the computation complexity decreases to $\mathcal{O}(N^m)$, which is $n-m$ times faster.

B. Inexact Reconstruction: ACS and Lipschitz CLF

Lemma 1 and Theorem 2 both provide exact reconstructions of the CLVF, but on different domains. In this section, we generalize to the case in which the subsystems have shared control, and therefore the sufficient condition in Theorem 2 is not met. Though exact reconstruction of a CLVF in the original state space is impossible, we can still reconstruct a Lipschitz continuous CLF and it ROES using the subsystems' CLVFs and ACSs. We remove the assumption that $\ell(x) = \max(\ell_1(z_1), \ell_2(z_2))$.

A key difference compared to the exact reconstruction is that we focus on $\mathcal{U}_a(x)$ for $V_\gamma^\infty(x)$, instead of $\mathbb{U}_a(x, t)$ for $V_\gamma(x, t)$. That is to say, we do not care about how the subsystems TV-CLVF evolve, but only care about its CLVF.

Note that for the CLVF, its ACS becomes time-independent:

$$\mathcal{U}_a(x) = \{u \in \mathcal{U} : D_x V_\gamma^\infty[f(x) + g(x) \cdot u] \leq -\gamma V_\gamma^\infty(x)\}. \quad (11)$$

Denote the ACSs for two subsystems as $\mathcal{U}_{a,1}(z_1), \mathcal{U}_{a,2}(z_2)$, and their shared control components as $\mathcal{U}_{a,1}^c(z_1)$ and $\mathcal{U}_{a,2}^c(z_2)$. The ACS for (1) can be reconstructed as

$$\begin{aligned} \bar{\mathcal{U}}_a(x) &= \mathcal{P}_{u,1}^{-1}(\mathcal{U}_{a,1}(\mathcal{P}_{x,1}(x))) \cap \mathcal{P}_{u,2}^{-1}(\mathcal{U}_{a,2}(\mathcal{P}_{x,2}(x))) \\ \bar{\mathcal{U}}_a^c(x) &= \mathcal{U}_{a,1}^c(\mathcal{P}_{x,1}(x)) \cap \mathcal{U}_{a,2}^c(\mathcal{P}_{x,2}(x)). \end{aligned}$$

Theorem 3: Let $\bar{V}_\gamma^\infty(x) = V_{\gamma,1}^\infty(z_1) + V_{\gamma,2}^\infty(z_2)$ where $z_1 = \mathcal{P}_{x,1}(x), z_2 = \mathcal{P}_{x,2}(x)$. Assume $\bar{\mathcal{U}}_a^c(x)$ is non-empty for all $x \in \bar{\mathcal{S}}_\gamma$, where $\bar{\mathcal{S}}_\gamma$ is some level set of \bar{V}_γ^∞ . Then, \bar{V}_γ^∞ is a Lipschitz continuous local CLF for (1) on $\bar{\mathcal{S}}_\gamma$.

Proof: From (4), there exist $v_1 \in \mathcal{U}_{a,1}(z_1)$ and $v_2 \in \mathcal{U}_{a,2}(z_2)$, such that

$$\begin{aligned} &D_x \bar{V}_\gamma^\infty(x) \cdot (f(x) + g(x) \cdot u) \\ &= D_x V_{\gamma,1}^\infty(z_1) \cdot (f_1(z_1) + g_1(z_1)v_1) + \\ &\quad D_x V_{\gamma,2}^\infty(z_2) \cdot (f_2(z_2) + g_2(z_2)v_2) \\ &\leq -\gamma V_{\gamma,1}^\infty(z_1) - \gamma V_{\gamma,2}^\infty(z_2) \\ &= -\gamma \bar{V}_\gamma^\infty(x), \end{aligned}$$

where $u = \mathcal{P}_{u,1}^{-1}(v_1) \cap \mathcal{P}_{u,2}^{-1}(v_2)$. In other words, $\forall x \in \bar{\mathcal{S}}_\gamma$, there exists some $u \in \mathbb{U}$ s.t. the Lie derivative along (1) is smaller than $-\gamma \bar{V}_\gamma^\infty(x)$.

Further, since both $V_{\gamma,1}^\infty$ and $V_{\gamma,2}^\infty$ are positive definite and all level sets are closed, $\bar{V}_\gamma^\infty(x) = V_{\gamma,1}^\infty + V_{\gamma,2}^\infty$ must also be positive definite and have closed level sets. We conclude that $\bar{V}_\gamma^\infty(x)$ is a local Lipschitz continuous CLF. ■

Similar to Proposition 1, system (1) can be exponentially stabilized to the origin from $\bar{\mathcal{S}}_\gamma$.

Remark 5: We use the summation instead of the maximum to reconstruct the value function. This is because using summation does not introduce additional non-differentiable points, whereas for the maximum, the reconstructed value function is non-differentiable for all x where $V_{\gamma,1}^\infty(z_1) = V_{\gamma,2}^\infty(z_2)$.

C. Optimal QP Controller

For both exact and inexact reconstruction, the controller that guarantees exponential stabilizability can be synthesized by solving the following QP,

$$\begin{aligned} &\min_{u \in \mathcal{U}} \|u - u_r\|_2^2 \\ \text{s.t. } &D_x \bar{V}_\gamma^\infty[f(x) + g(x) \cdot u] \leq -\gamma \bar{V}_\gamma^\infty(x), \quad (12) \end{aligned}$$

where u_r is the reference control input. This QP is guaranteed to be feasible on \mathcal{D}_γ (or \mathcal{S}_γ) [6]. For systems whose CLVFs can be exactly reconstructed, the constraints in (12) can either be solved directly from the reconstructed CLVF, or from subsystems CLVFs. For systems in which the CLVFs cannot be exactly reconstructed, the control can be determined by solving (12) with the reconstructed CLF.

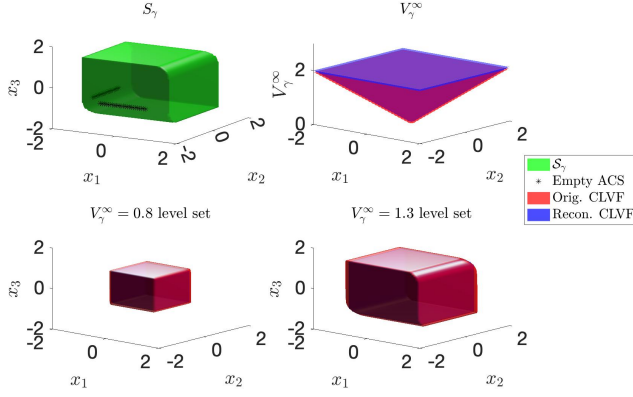


Fig. 2. Original and reconstructed CLFVs with $\gamma = 0.1$ for system (14). Top left, S_γ for the reconstructed ACS produced by Alg. 1. Top right, comparison of the reconstructed and original CLVF projected into $x_1 - x_2$ plane. Bottom, different level sets of original and reconstructed CLFVs. The reconstructed CLVF is identical to the original CLVF in S_γ , validating Theorem 2. The computation time for the original system's CLVF is 102s on a grid of $[-2, -2, -2]$ to $[2, 2, 2]$ with 61 grid points on each dimension. On the same grid, the computation time for the subsystems' CLFVs is 3.37s, and the computation of S_γ takes 0.86s. Combined, the decomposition speeds computation time by 30x.

IV. NUMERICAL EXAMPLE

In this section, we provide numerical examples that validate our theory. This includes three toy examples in low dimensions that validates the theory, and one practical 10D quadrotor system. For simplicity, in all examples, the loss function is chosen to be the infinity norm. All simulations are conducted using MATLAB and tool boxes [18], [19].

A. 2D System (Lemma 1)

Consider the following 2D system

$$\dot{x}_1 = x_1^2 + u_1, \quad \dot{x}_2 = x_2 + u_2, \quad (13)$$

where $u_1 \in [-4, 4]$ and $u_2 \in [-1, 1]$. The two states evolve purely on their own, therefore each state's dynamics is one subsystem. We compute the CLVF for both subsystems and also directly for the original system with $\gamma = 0.1$. The results are shown in Fig. 1.

B. 3D System (Theorem 2)

Consider the following 3D system

$$\dot{x}_1 = x_3 + u_1, \quad \dot{x}_2 = x_3 + u_2, \quad \dot{x}_3 = u_3, \quad (14)$$

where $u_1, u_2 \in [-1, 1]$ and $u_3 \in [-0.5, 0.5]$ are the control inputs. Take $z_1 = [x_1, x_3]$, $z_2 = [x_2, x_3]$, and $v_1 = [u_1, u_3]$, $v_2 = [u_2, u_3]$, we can decompose the system into two 2D subsystems. We can apply Alg. 1 to find the domain S_γ , such that if initialized inside, the system will stabilize to its equilibrium point. The results are shown in Fig. 2.

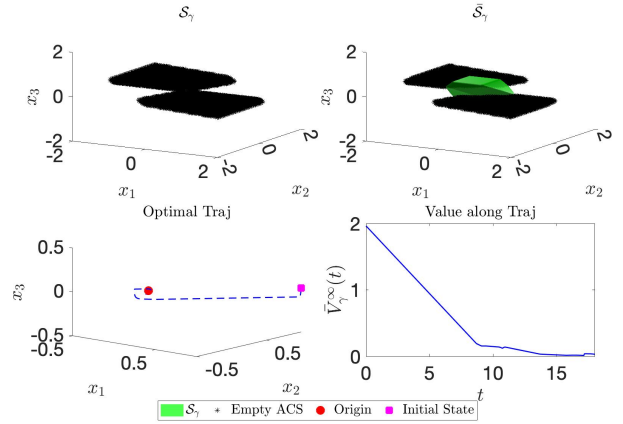


Fig. 3. Top: The black stars denote the states with empty ACS (and ACSs). Left, S_γ (consists only of the origin) computed from Alg. 1, shown in green. Right, \bar{S}_γ . Bottom left: trajectory simulation using the QP (12). Bottom right: decay of the CLF value along the trajectory. When initialized inside \bar{S}_γ , the system can be stabilized to the origin, validating Theorem 3. The computation time for the subsystems' CLFVs is 15.5s with a grid from $[-2, -2]$ to $[2, 2]$ and 101 nodes on each dimension. The computation of S_γ takes 3.26s.

C. 3D System (Theorem 3)

Consider the following 3D system

$$\dot{x}_1 = x_3, \quad \dot{x}_2 = x_3, \quad \dot{x}_3 = u, \quad (15)$$

where $u \in [-1, 1]$ is the control inputs. Take $z_1 = [x_1, x_3]$, $z_2 = [x_2, x_3]$, and $v_1 = [u_1, u_3]$, $v_2 = [u_2, u_3]$, we can decompose the system into two 2D subsystems. Applying Alg. 1, we find that S_γ is empty (top left of Fig. 3), which means the exact reconstruction is not possible. However, \bar{S}_γ is not empty (top right of Fig. 3), which means we could use Theorem. 3 to obtain a Lipschitz continuous CLF. A trajectory starting inside \bar{S}_γ and converging to the origin and the value along this trajectory is shown in Fig. 3 bottom.

D. 10D Quadrotor

Consider the 10D quadrotor system:

$$\begin{aligned} \dot{x}_1 &= x_2, & \dot{x}_2 &= g \tan x_3, & \dot{x}_3 &= -d_1 x_3 + x_4, \\ \dot{x}_4 &= -d_0 x_3 + n_0 u_1, & \dot{x}_5 &= x_6, & \dot{x}_6 &= g \tan x_7, \\ \dot{x}_7 &= -d_1 x_7 + x_8, & \dot{x}_8 &= -d_0 x_7 + n_0 u_2, \\ \dot{x}_9 &= x_{10}, & \dot{x}_{10} &= u_3, \end{aligned} \quad (16)$$

where (x_1, x_5, x_9) denote the position, (x_2, x_6, x_{10}) denote the velocity, (x_3, x_7) denote the pitch and roll, (x_4, x_8) denote the pitch and roll rates, and (u_1, u_2, u_3) are the controls. The system parameters are set to be $d_0 = 10, d_1 = 8, n_0 = 10, k_T = 0.91, g = 9.81, |u_1|, |u_2| \leq \pi/4, u_3 \in [-1, 1]$.

This 10D system can be decomposed into three subsystems: X subsystem with states $[x_1, x_2, x_3, x_4]$, Y subsystem with states $[x_5, x_6, x_7, x_8]$, and Z subsystem with states $[x_9, x_{10}]$. It can be verified that all three subsystems have an equilibrium point at the origin. Further, there's no shared

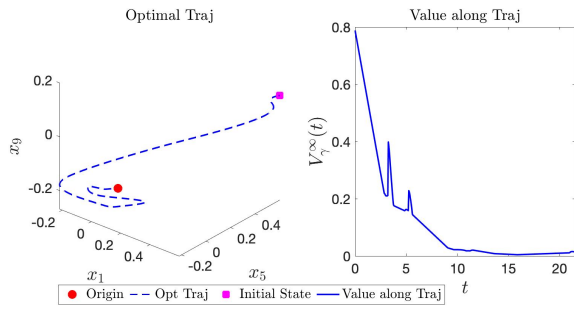


Fig. 4. Since the CLVF is a 10D function, we do not visualize it, but show instead a trajectory that is stabilized to the origin and the value decay along this trajectory. The computation for the X/Y subsystem takes 1374.51s on a grid with 17 grid points each dimension, and 56.63s for the Z subsystem, with 151 grids each. The direct computation for the 10D CLVF is not tractable : creating the 10D grid exceeds the MATLAB memory limit and therefore is not allowed.

control or states among subsystems, therefore, Lemma 1 can be used to exactly reconstruct the CLVF using $\bar{\ell}(x) = \|x\|_\infty$. The result is shown in Fig. 4.

V. CONCLUSION

In this paper, we presented an exact and inexact reconstruction method for CLVFs by leveraging ACS, providing a corresponding QP controller, and identifying the domain that can exponentially stabilize the system. We validate our method with a nonlinear 2D system with no shared control for exact reconstruction, as well as a multi-input linear 3D system for the shared control case. Further, we validate the inexact reconstruction method with the single-input linear 3D system by finding the corresponding domain. Lastly, a 10D quadrotor example is provided, showing numerical efficiency.

Through this method, we can scalably compute higher-dimensional CLVFs for a class of nonlinear systems. Future work includes validating high-dimensional CLVFs through neural solvers like DeepReach [11], applying this method to online trajectory planning problems, finding the “smallest control invariant set” defined in the original CLVF work [6], and exploring more on the region where the reconstructed ACS is empty.

REFERENCES

- [1] E. D. Sontag, “A ‘universal’ construction of artstein’s theorem on nonlinear stabilization,” *Systems & control letters*, vol. 13, no. 2, pp. 117–123, 1989.
- [2] R. A. Freeman and J. A. Primbs, “Control lyapunov functions: New ideas from an old source,” in *Proceedings of 35th IEEE conference on decision and control*, vol. 4. IEEE, 1996, pp. 3926–3931.
- [3] F. Camilli, L. Grüne, and F. Wirth, “Control lyapunov functions and zubov’s method,” *SIAM Journal on Control and Optimization*, vol. 47, no. 1, pp. 301–326, 2008.
- [4] P. Ogren, M. Egerstedt, and X. Hu, “A control lyapunov function approach to multi-agent coordination,” in *Proceedings of the 40th IEEE Conference on Decision and Control (Cat. No. 01CH37228)*, vol. 2. IEEE, 2001, pp. 1150–1155.
- [5] Z. Artstein, “Stabilization with relaxed controls,” *Nonlinear Analysis: Theory, Methods & Applications*, vol. 7, no. 11, pp. 1163–1173, 1983.
- [6] Z. Gong, M. Zhao, T. Bewley, and S. Herbert, “Constructing control lyapunov-value functions using hamilton-jacobi reachability analysis,” *IEEE Control Systems Letters*, vol. 7, pp. 925–930, 2022.

- [7] Z. Gong and S. Herbert, “Robust control lyapunov-value functions for nonlinear disturbed systems,” *arXiv preprint arXiv:2403.03455*, 2024.
- [8] L. C. Evans and P. E. Souganidis, “Differential games and representation formulas for solutions of hamilton-jacobi-isaacs equations,” *Indiana University mathematics journal*, vol. 33, no. 5, pp. 773–797, 1984.
- [9] S. Bansal, M. Chen, S. Herbert, and C. J. Tomlin, “Hamilton-jacobi reachability: A brief overview and recent advances,” in *Proceedings of 56th IEEE conference on decision and control*. IEEE, 2017, pp. 2242–2253.
- [10] J. F. Fisac, N. F. Lugovoy, V. Rubies-Royo, S. Ghosh, and C. J. Tomlin, “Bridging hamilton-jacobi safety analysis and reinforcement learning,” in *Proceedings of 36th IEEE International Conference on Robotics and Automation*. IEEE, 2019, pp. 8550–8556.
- [11] S. Bansal and C. J. Tomlin, “Deepreach: A deep learning approach to high-dimensional reachability,” in *Proceedings of 38th IEEE International Conference on Robotics and Automation*. IEEE, 2021, pp. 1817–1824.
- [12] M. Chen, S. Herbert, and C. J. Tomlin, “Exact and efficient hamilton-jacobi guaranteed safety analysis via system decomposition,” in *Proceedings of 34th IEEE International Conference on Robotics and Automation*. IEEE, 2017, pp. 87–92.
- [13] M. Chen, S. L. Herbert, M. S. Vashishtha, S. Bansal, and C. J. Tomlin, “Decomposition of reachable sets and tubes for a class of nonlinear systems,” *IEEE Transactions on Automatic Control*, vol. 63, no. 11, pp. 3675–3688, 2018.
- [14] S. L. Herbert, S. Bansal, S. Ghosh, and C. J. Tomlin, “Reachability-based safety guarantees using efficient initializations,” in *Proceedings of 58th IEEE conference on decision and control*. IEEE, 2019, pp. 4810–4816.
- [15] J. Liu, P. Zhao, Z. Gan, M. Johnson-Roberson, and R. Vasudevan, “Leveraging the template and anchor framework for safe, online robotic gait design,” in *Proceedings of 37th IEEE International Conference on Robotics and Automation*. IEEE, 2020, pp. 10 869–10 875.
- [16] P. Holmes, S. Kousik, B. Zhang, D. Raz, C. Barbalata, M. Johnson-Roberson, and R. Vasudevan, “Reachable sets for safe, real-time manipulator trajectory design,” *arXiv preprint arXiv:2002.01591*, 2020.
- [17] C. He, Z. Gong, M. Chen, and S. Herbert, “Efficient and guaranteed hamilton-jacobi reachability via self-contained subsystem decomposition and admissible control sets,” *IEEE Control Systems Letters*, vol. 7, pp. 3824–3829, 2023.
- [18] I. M. Mitchell and J. A. Templeton, “A toolbox of hamilton-jacobi solvers for analysis of nondeterministic continuous and hybrid systems,” in *International workshop on hybrid systems: computation and control*. Springer, 2005, pp. 480–494.
- [19] M. Chen, S. Herbert, S. Bansal, and C. Tomlin, “Optimal control helper toolbox,” URL <https://github.com/HJReachability/helperOC>.